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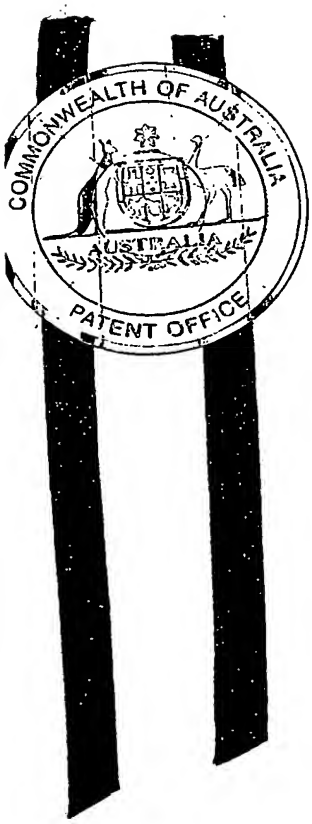

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PROVISIONAL SPECIFICATION

Invention Title: "Pulse sequences for exciting nuclear quadrupole resonance"

The invention is described in the following statement:

"Pulse sequences for exciting nuclear quadrupole resonance"

Field of the Invention

The present invention relates to the practical use of the nuclear quadrupole resonance (NQR) phenomenon for identifying substances that contain quadrupole nuclei with either integer or half-integer spins, particularly for identifying explosive or narcotic substances.

More particularly the invention refers to multi-pulse RF excitation of quadrupole nuclei and to the subsequent measurement of the NQR signal under the conditions when the temperature of the sample containing quadrupole nuclei is unknown.

Throughout the specification, unless the context requires otherwise, the word "comprise" or variations such as "comprises" or "comprising", will be understood to imply the inclusion of a stated integer or group of integers but not the exclusion of any other integer or group of integers.

The term "preparatory pulse" means both a separate preparatory pulse and a group of preparatory pulses.

The term "a group of preparatory pulses" means a group of pulses that precede a multi-pulse sequence distributed within time interval $\leq 3T_{1\rho}$ ($T_{1\rho}$ being the time of spin-lattice relaxation in a rotating coordinate system), during which the NQR signal, as a rule, is not measured.

The term "the body of the sequence" is used to signify a multi-pulse sequence with subtracted preparatory pulses; the measurement of an NQR signal usually occurring when the "body of the sequence" is in action.

Background Art

The following discussion of the background art is intended to facilitate an understanding of the present invention only. It should be appreciated that the discussion is not an acknowledgement or admission that any of the material referred to is or was part of the common general knowledge in Australia as at the priority date of the application.

For the purposes of pulsed NQR, any solid sample containing quadrupole nuclei can be characterised by three parameters: the spin-lattice relaxation time T_1, the spin-spin relaxation time T_2 and the time of the induction signal damping T_2^*.

From the point of view of practical use in NQR, and on the basis of the above parameters, the following classification of multi-pulse sequences can be constructed:

1. Single pulse sequences, which can include multi-pulse sequences of any type, if intervals between the pulses in these sequences exceed the spin-lattice relaxation time T_1.

2. Sequences with intervals between pulses τ that are within the limits $T_2^* < \tau << T_1$. All echo-sequences (sequences composed of a certain number of pulses which are organised in such a way that the NQR signal is formed not directly after the radio frequency irradiation pulse, but after a certain delay, necessary for refocussing the magnetic momentum of the sample nuclei) could also be regarded as belonging to this type of sequence, because for the optimal formation of the echo signal the condition $T_2^* < \tau < T_2$ should hold true. One of the main peculiarities of this type of sequence is its capability to saturate the quadrupolar spin system of the sample. This can be observed when a multi-pulse sequence of this type is used, as the chain of NQR signals measured in the observation windows between the pulses decays with a time constant T_{1e}, which is called the

effective relaxation time and lies within the limits of $T_2 \le T_{1e} < T_1$ (or, to be more precise, within the limits of $T_2 \le T_{1e} < T_{1\rho}$, where $T_{1\rho}$ is the relaxation time in rotating frame, with the permanent condition of $T_{1\rho} < T_1$).

3. Stochastic sequences.

4. Multi-pulse sequences of the Steady State Free Precession (SSFP) type. Intervals between pulses in these sequences (τ) fulfil the condition of $\tau < T_2^*$. This type can include quite complex formations, containing not only SSFP sequences but also special techniques for destroying the SSFP state; this "destruction" can be achieved by including the magnetic field gradient pulses, by using composite pulses, by forming a special phase alternation of the RF carrier frequency, etc. The purpose of this "destruction" is to overcome one of the main drawbacks of SSFP sequences - intensity anomalies, which manifest themselves by the decreasing amplitude and the increasing rate of signal decay when the parameters of an irradiating sequence approach resonance conditions $n \cdot \omega_{ef} = m \cdot \frac{\pi}{\tau}$, where τ is the interval between pulses of the sequence, n and m are whole numbers, an effective field ω_{ef} substitutes the effect of the RF pulses and the resonance offset

5. Complex types of multi-pulse sequences containing sub-sequences of two or more of the above types of multi-pulse sequences.

It should be appreciated, however, that this classification omits borderline cases.

As the fifth group does not have any individual physical characteristics that do not relate to at least one of the previous groups, further analysis of only the peculiarities of the first four groups of sequences in the above classification will hereinafter be considered.

<u>Group I</u>

Advantages:

1. No intensity anomalies;

2. No saturation problem, and therefore no signal decay.

Disadvantages:

1. At long T_1 times the detection time of a sample can exceed any practically acceptable limits;

2. Single pulses can only create a free induction decay (FID) signal, entirely determined - as well as magneto-acoustic ringing, piezo-electric effects and the spurious signals of the resonance circuit of the NQR detector probe - by the pulse that generated it. The consequence of this is that the NQR signal measured when the standard means of damping spurious signals is used, is considerably weakened, and often disappears completely.

Because of these disadvantages the first group of sequences is of little benefit for practical use in NQR.

Group II

Advantages:

1. Possibility of generating echo-signals with parameters depending not only on the last pulse but also on the preceding pulses of the sequence which can be used to cancel spurious signals while keeping and sometimes even increasing the intensity of the NQR signal;

2. Possibility of generating echo-signals at times exceeding "dead time" of the receive system of the spectrometer;

3. Possibility of saturating the sample, which enables the measurement of the spurious signals together with the NQR signals, then spurious signals only, after which the latter can be subtracted.

Disadvantages:

1. Time available for accumulating the NQR signal is limited by the time constant $T_{1e} < T_1$;

2. The use of echo sequences (the possibility of which is one of the main advantages of this group), does not help to detect a number of substances that have a little or zero asymmetry parameter, as the amplitude of echo-signals decreases with the decrease of the asymmetry parameter.

Group III

Advantages:

1. No intensity anomalies;

2. Possibility of saturating the sample to enable subtraction of spurious signals. Saturation in this case is entirely determined by the flip angle of the pulses and the time of spin-lattice relaxation T_1;

3. The stochastic resonance requires lower peak power. The peak power can be tens and even hundreds times lower than when using coherent pulses and still achieve similar sensitivity.

Disadvantages:

1. Stochastic sequences belong to saturating sequences; however the saturation of the spin system limits the time of the NQR signal accumulation, as is the case with Group II sequences, which is equivalent to a loss of sensitivity; it

does not produce the advantages that Group II sequences can offer using echo signals.

2. Using a stochastic sequence for saturating a sample does not give any advantages as compared with normal saturation methods that use coherent pulses, but is technically more complicated to realise.

3. Using stochastic sequences requires introducing a random delay in the timing of the radio frequency pulses, but there are cases where the timing between radio frequency pulses is relatively short and any delays introduced in the timing tend to greatly increase the spectrometer time required to obtain the desired time average spectral data.

The general conclusion about the use of stochastic sequences in NQR for identification of explosive and narcotic substances is that they are more technically complicated to produce and the achieved sensitivity as a rule does not exceed that of coherent sequences.

Group IV

Advantages:

1. A possibility to receive a continuous chain of signals if the requirement $n \cdot \omega_{\sigma} \neq m \cdot \frac{\pi}{\tau}$ is met, and this ensures unlimited time for signal accumulation;

2. A possibility to receive an NQR signal phase different from the phase of irradiating pulses, which can be used for cancelling intensity anomalies, or for subtracting spurious signals;

3. Comparatively little RF power is sufficient for detecting samples in big volumes.

Disadvantages:

1. Intensity anomalies;

2. Higher requirements to the time of damping ringing and the time of equipment insensitivity at short T_2^*.

The first of the above disadvantages makes the SSFP group sensitive to the changes in the resonance frequency of the quadrupole spin system during temperature changes. If the temperature of the sample leads to the setting of such frequency ω_Q of the quadrupole transition in the sample that the resonance condition $n \cdot \omega_{eff} = m \cdot \frac{\pi}{\tau}$ is met, then the chain of the NQR signals decays with time constant T_{1c}, which is the function of the frequency offset, pulse interval and the flip angle. At short T_1 times ($T_{1c} < T_1$) the decay happens quickly, decreasing sharply the sensitivity of detection.

For a number of substances temperature dependence of the resonance frequencies of quadrupolar nuclei is quite considerable. For example, for RDX at frequency $\nu_+ = 5.192$ MHz at temperatures close to room temperature, the change in ^{14}N resonance frequency is -520 Hz/°K, for PETN at the ^{14}N frequency $\nu_+ = 890$ kHz it is -160 Hz/°K, for KNO_3 at nitrogen-14 line $\nu_+ = 567$ kHz it is -140 Hz/°K etc.

The maximum sensitivity in most cases is achieved in practice when using SSFP sequences, which if the parameters are properly chosen permit achievement of the biggest signal to noise ratio in unit time.

The first SSFP sequence consisting of identical coherent RF pulses was used in NMR in 1951 and later studied in great detail. In NQR, this sequence was first used for measuring the T_1 of the ^{14}N resonance line in hexamethylene tetramine. Then a two-frequency version of this sequence was used to measure relaxation times in urea, which involved the simultaneous irradiation of the two ^{14}N resonance transitions ν_+ and ν_- with two SSFP sequences.

Later, a sequence with identical coherent RF pulses and a nonzero resonance offset was used. Then some combinations of SSFP sequences were used to solve the problem of intensity anomalies in detecting explosives by the NQR method.

The following method of suppressing intensity anomalies was suggested.

To irradiate the sample, the basic version of the SSFP sequences was used – a sequence of coherent equally spaced pulses with a flip angle φ and the repetition cycle τ : $[\tau/2-\varphi-\tau/2]_n$, where n is the number of the sequence cycles (it is also possible to write it down as $[\varphi-\tau]_n$).

The irradiation was done with different series of pulses, with the carrier frequency of pulses in each series corresponding to one of the two values: f_0 and $f_0 \pm \frac{2}{\tau}$,

where f_0 is the frequency close to the resonance frequency.

If there was no signal when irradiating with the series that had the carrier frequency f_0, the sample would then be irradiated with the other series with the carrier frequency $f_0 \pm \frac{2}{\tau}$.

The difference in the frequency of both carrier frequencies corresponds to the difference between the frequencies at which the maximum and the minimum signal intensity was observed.

It was then suggested to use combinations of sequences with phase alternating (PAPS) and without phase alternating (NPAPS): $[\varphi_x-\tau-\varphi_x-\tau]_n[\varphi_x-\tau-\varphi_{-x}-\tau]_n$,

where the bottom index at the flip angle sign φ designates the phase of the carrier frequency for the RF pulse, and n is the number of cycles of the sequence.

In this case, if in the intervals corresponding to PAPS, the maximum signal was achieved, then in the intervals corresponding to NPAPS, the minimum signal would be observed. Such sequence combinations permitted irradiating the sample without switching the carrier frequency.

Essentially, two separate methods were proposed by which to perform the signal accumulation.

In the first method, the signals received after φ_x pulses of the NPAPS sequence and after φ_{-x} pulses of the PAPS sequence are subtracted, and those received after φ_x of the PAPS sequence are added together. This allows not only a decrease in intensity anomalies, but also elimination of magneto-acoustic ringing.

In the second method, the signals received after φ_x pulses of both PAPS and NPAPS sequences are added up with the positive sign, and after φ_{-x} pulses they are added with the negative sign.

The maximum accumulated signal achieved by using either method of accumulation is less than the maximum achieved when using only NPAPS or PAPS by $\sqrt{2}$ times.

For the sake of comparison, as shown in FIG. 1, the curves corresponding to two dependencies of NQR signal on the frequency received for $NaNO_2$ are shown, after irradiation with NPAPS and PAPS sequences using the accumulation rules determined by the first method described above (curve 1) and the second method (curve 2), respectively.

Thus all methods described above for eliminating temperature effects associated with intensity anomalies at a prescribed number of accumulations result in decreasing the intensity of the measured signal, as compared with the maximum signal intensity possible to measure that would arise from using only one of the SSFP sequences.

Disclosure of the Invention

The principal object of the present invention is to increase the accuracy of detection of prescribed substances such as, but not limited to, certain explosives and narcotics, in specimens, compared with previously known methods of detecting same using NQR, by reducing temperature effects and increasing the NQR signal intensity.

In accordance with one aspect of the invention, this object is generally achieved by using a combination of two or more sequences, arranged so that a definite regularity of the phase alteration of RF pulses in each of the sequences is equivalent to a shift of spectral components of the sequences in relation to each other, and in at least one of the sequences, not less than two phases are alternating, and at least one of the sequences contains a preparatory pulse or group of preparatory pulses.

Thus, according to a preferred arrangement of this aspect of the invention, there is provided a method of detecting a class of explosive or narcotic substances containing quadrupolar nuclei in a sample using nuclear quadrupole resonance, including the following steps:

generating a combination of the steady state free precession RF pulse sequences with a preparatory pulse or group of preparatory pulses, the RF pulse sequences consisting of pulses that contain phases of the carrier frequency chosen from a certain set of unmatched phases distributed within the interval from 0 to 2π radian, with every sequence different from the others either by the number of phases chosen from the set, or by the sequence order inside the sequence; and

irradiating the sample with said combination of the RF pulse sequences.

Preferably, the method includes detecting nuclear quadrupole resonance signals when the combination of the RF pulse sequences irradiates the sample; and

combining all said nuclear quadrupole resonance signals to generate the resulting signal.

Preferably, the predetermined frequency of the RF pulse sequence is near to one of the NQR frequencies of the substances to be detected.

In accordance with another aspect of the invention, the reduction in the temperature effects is achieved by using a combination of two or more sequences different from a combination of PAPS and NPAPS, arranged so that a definite regularity of the phase alteration of RF pulses in each of the sequences is equivalent to a shift of spectral components of the sequences in relation to each other, and in at least one of the sequences not less than two phases are alternating and none of the sequences contains a preparatory pulse or group of preparatory pulses.

According to a preferred arrangement of this other aspect of the invention, there is provided a method of detecting a class of explosive or narcotic substances containing quadrupolar nuclei in a sample using nuclear quadrupole resonance, including the following steps:

generating a combination of the steady state free precession RF pulse sequences without a preparatory pulse or group of preparatory pulses, using a combination of two or more sequences different from a combination of PAPS and NPAPS, the RF pulse sequences consisting of pulses that contain phases of the carrier frequency chosen from a certain set of unmatched phases distributed within the interval from 0 to 2π radian, with every sequence different from the others either by the number of phases chosen from the set, or by the sequence order inside the sequence; and

irradiating the sample with the combination of the RF pulse sequences.

Preferably, the method includes detecting nuclear quadrupole resonance signals when the combination of the RF pulse sequences irradiates the sample; and

combining all said nuclear quadrupole resonance signals to generate the resulting signal.

In a preferred aspect of the invention, the purpose of the invention is achieved by completing one measurement act using a combination that consists of at least two multi-pulse sequences having the same carrier frequency of the RF pulses, but different phase shifts between pulses in each sequence of the said combination. This results in all the sequences of the combination having a different effective carrier frequency, and, consequently, the NQR signals obtained after each of the sequences having a different dependence on the frequency offset. If we combine the NQR signals from different sequences, the resulting signal's intensity has a significantly reduced dependence on the frequency offset and, consequently, temperature effects.

Preferably, it is important also to consider that any spin system has a non-zero "phase memory" time. The phenomenon of "phase memory" manifests itself in the fact that a sudden momentary perturbation of the spin system influences its evolution for a certain period of time. This phenomenon can be used to change the dependence of the NQR signal on the frequency offset to reduce the temperature effects. For this purpose preparatory pulses (or groups of preparatory pulses) may be used that are switched on before one or several sequences of the combination.

Brief Description of the Drawings

The invention will be better understood in the light of the following description of two preferred embodiments thereof. The description is made with reference to the accompanying drawings, wherein:

FIG.1 is a graph representing curves corresponding to two dependencies of the intensity of NQR signals plotted against the resonance frequency offset in kHz, whereby the NQR signals are on the frequency received for $NaNO_2$, which is on line $\nu_- = 3.603\ \mathrm{MHz}$, after NPAPS and PAPS sequences action with the rules of

summing up determined respectively by the first method (curve 1) and the second method (curve 2), as described in the background art;

FIG.2 is a graph similar to Fig 1, but demonstrating examples of the influence of preparatory pulses on the value of the NQR signal, where the preparatory pulses are switched on before the PAPS sequence:

$$\varphi_{0\phi} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-x} - t_{delay} - T_{acq(-x)})_n ;$$

FIG.3 is another graph, similar to Figs 1 and 2, but showing an example of using PAPS and NPAPS sequences with preparatory pulses at frequency ν_- for $NaNO_2$, wherein:

Curve 1 corresponds to PAPS and NPAPS sequences with preparatory pulses:

$\varphi_{0x} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-x} - t_{delay} - T_{acq(-x)})_n$, and $\varphi_{0y} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)})_{2n}$;

and curve 2 is the result of an experiment with these sequences with the same number of accumulations but without preparatory pulses, corresponding to the second method described in relation to the background art;

FIG.4 is a graph similar to those of the preceding figures, but showing the result of using four sequences of the type for powdered RDX at the transition frequency $\nu_- = 3.410\ \text{MHz}$ also in accordance with the first embodiment, the sequences being:

$$\varphi_{0y} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)})_{4m} ;$$

$$\varphi_{0x} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-x} - t_{delay} - T_{acq(-x)})_{2m} ;$$

$$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_y - t_{delay} - T_{acq(+y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)})_m ;$$

$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_y - t_{delay} - T_{acq(+y)})_m$.; and

FIG.5 is a graph similar to those of the preceding figures, but showing two examples of using a combination of sequences without preparatory pulses in accordance with the second embodiment, the sequences being :

$(\varphi_x - t_{delay} - T_{acq} - \varphi_y - t_{delay} - T_{acq} - \varphi_{-x} - t_{delay} - T_{acq} - \varphi_{-y} - t_{delay} - T_{acq})_m$, and

$(\varphi_x - t_{delay} - T_{acq} - \varphi_{-y} - t_{delay} - T_{acq} - \varphi_{-x} - t_{delay} - T_{acq} - \varphi_y - t_{delay} - T_{acq})_m$; wherein the experiments were carried out using RDX at the frequency line $\nu_- = 3.410$ MHz.

Best Mode(s) for Carrying Out the Invention

For reducing temperature effects, "bodies of sequences" must contain pulses with various sets of the carrier frequency phases.

As the effective carrier frequency of the sequence does not depend on the absolute value of the RF pulses phase, but only on the difference between phases of adjacent pulses divided by the time interval between these pulses, all phases are calculated from the phase of the first pulse of the body of the sequence, which, irrespective of its actual value, will always be considered to be zero.

Firstly, a group consisting of N ($N \geq 2$) different phases, containing all the phases of one combination of multi-pulse sequences, will be considered, the phases being:

$$\phi_1, \phi_2, \ldots \phi_i, \ldots \phi_N. \qquad (1)$$

All phases ϕ_i, i=1 .... N are within the interval from 0 to 2π radian, $\phi_i \neq \phi_j$ if $i \neq j$ and $\phi_1 = 0$.

The body of each pulse sequence must contain pulse cycles (at least one), with the pulses of each cycle containing one of the following N! sets of the carrier frequency phases:

one set of phases being of the type: $\phi 1_1$, $\phi 1_2$, ... $\phi 1_i$, ... $\phi 1_N$;

N sets of phases being of the type: $\phi 2_1$, $\phi 2_2$, ... $\phi 2_i$, ... $\phi 2_{N-1}$;

: :

: :

$\frac{N!}{(N-i)!i!}$ sets of phases being of the type: ϕi_1, ϕi_2, ... ϕi_i, ... ϕi_{N-i};

: :

: :

N sets of phases being of the type: ϕN_1.

Here each phase ϕi_k $(i, k = 1, \ldots N)$ is one of a set of phases (1), with $\phi i_k \neq \phi i_m$, if $k \neq m$. The set $\phi 1_k$ is equivalent to the set ϕ_k.

If the bodies of all sequences used in one detection process contain the same set of phases they must differ from each other by at least the order of alternation of the pulse phases.

Thus the best mode for carrying out the present invention is concerned with improving the detection of substances with relaxation time T_1 comparable with the time of the duration of the pulse sequence.

To explain the influence of a preparatory pulse included in the SSFP sequence, consideration will now be made of the peculiarities of this type of sequence in detail.

The development of the spin system of the sample from the moment the multi-pulse irradiation started, undergoes three main stages:

(1) transient processes;

(2) quasi-stationary state;

(3) stationary state.

As a rule, transient processes decay at times $t \leq 3T_2$, and are replaced by a quasi-stationary state.

One of the peculiarities of the quasi-stationary state as compared with the stationary state proper, which replaces it at times $\leq 3T_{1\rho}$ ($T_{1\rho}$ is the time of spin-lattice relaxation in the rotating frame), is the presence of the "phase memory" which manifests itself by the spin-system "remembering" the effect of the preparatory pulse. After the time $3T_{1\rho}$ the spin-system adopts the completely stationary state and on meeting the condition of $n \cdot \omega_{eff} \neq m \cdot \frac{\pi}{\tau}$ a different from zero NQR signal exists as long as it is needed.

The fact that the "phase memory" of the spin system is limited by the time interval being $\leq 3T_{1\rho}$, explains the definition of the "group of preparatory pulses" provided above.

One of the features of the first embodiment of the best mode for carrying out the present invention is the use of the quasi-stationary state to "remember" the effect of the preparatory pulse for increasing the intensity of the NQR signal and at the same time reducing the temperature effects.FIG.2 shows examples of the influence of preparatory pulses used prior to the PAPS sequence $\varphi_{0\phi} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-x} - t_{delay} - T_{acq(-x)})_n$ upon the value of the NQR signal. The duration of the multi-pulse sequence in these examples is less than the spin-lattice relaxation time T_1. Here φ_0 is the flip angle of the preparatory pulse; φ is

the flip angle of the pulses of the sequence body; ϕ is the phase of the preparatory pulse; t_{delay} is the time of the delay exceeding the "dead time" of the receiver system; $T_{acq(\theta)}$ is acquisition time; θ is the receiver phase. The duration of the multi-pulse sequence in these examples is less than the spin-lattice relaxation time T_1. Experiments were carried out on a sample of $NaNO_2$ on line ν_-. In all cases the experiments were carried out at room temperature. Curve 1 was received at $\varphi_0 = \pi/2$ and $\phi = +x$, curve 2 was received without the preparatory pulse, and curve 3 was received at $\varphi_0 = \pi/2$ and $\phi = +y$.

According to the first embodiment for carrying out the invention, the increased intensity of the NQR signal with simultaneous elimination of intensity anomalies is achieved using two and more SSFP type sequences, arranged so that a definite regularity of the phase alteration of RF pulses in each of the sequences is equivalent to a shift of spectral components of the sequences in relation to each other, and in at least one of the sequences, not less than two phases are alternating, and at least one of the sequences contains a "preparatory pulse" or a "group of preparatory pulses".

The particular apparatus for producing pulse sequences of this kind is known, and described in the applicant's corresponding International Patent Application PCT/AU00/01214 (WO 01/25809). which is incorporated herein by reference. Accordingly, the apparatus for producing the pulse sequences will not be further described herein.

FIG.3 and 4 shows two examples of the use of the first embodiment.

In both examples the magnetic field component B_1 of the RF pulses was 4.5 Gauss. The duration of the 90^0 pulse in the powder sample was $68\ \mu s$. Experiments were conducted on $NaNO_2$ at the frequency $\nu_- = 3.603$ MHz at room temperature. The spin-lattice relaxation time for this line was $T_1 = 280$ ms.

FIG.3 shows an example of using PAPS and NPAPS sequences with preparatory pulses. Curve 1 corresponds to the PAPS and NPAPS sequences with preparatory pulses, and curve 2 shows experimental results for the same sequences with the same number of accumulations but without the preparatory pulses (as in the second method described previously with respect to the background art).

The duration of each sequence was less than 170 ms, and the interval between the sequences was 2 s.

The parameters of the sequences NPAPS $\varphi_{0y} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)})_{2n}$ and PAPS $\varphi_{0x} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-x} - t_{delay} - T_{acq(-x)})_n$ are as follows:

$\varphi_0 = \varphi = 90^\circ$; pulse duration $t_w = 68\ \mu s$; $\tau = 778 \mu s$; $t_{delay} = 600 \mu s$; $T_{acq(\theta)} = 1024 \mu s$; $n = 80$.

Now adopting the designations: $T = t_w + t_{delay} + T_{acq(\theta)}$; and where f_0 is the carrier frequency of the RF pulses, then the effective carrier frequencies f_{eff} for both sequences would be

$f_{eff} = f_0$ for NPAPS sequence;

$f_{eff} = f_0 + \frac{1}{2T}$ for PAPS sequence.

As can be seen from FIG.3, the use of preparatory pulses does not allow an increase in the intensity of the NQR signal at the minimum points, but beyond the narrow areas, near the minimum, the signal intensity is considerably increased.

FIG.4 shows the result of using four sequences for detecting powdered RDX, the sequences being of the following type:

$$\varphi_{0y} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)})_{4m}; \quad (2)$$

$$\varphi_{0x} - \tau - (\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-x} - t_{delay} - T_{acq(-x)})_{2m}; \quad (3)$$

$$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_y - t_{delay} - T_{acq(+y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)})_m; \quad (4)$$

$$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_y - t_{delay} - T_{acq(+y)})_m. \quad (5)$$

For all the four sequences $m = 50$, the duration of delays, pulses and acquisition times coincides completely with the previous example. The intervals between sequences are also 2 s.

The effective carrier frequencies are as follows:

$f_{eff} = f_0$ for sequence (2);

$f_{eff} = f_0 + \frac{1}{2T}$ for sequence (3);

$f_{eff} = f_0 + \frac{1}{4T}$ for sequence (4);

$f_{eff} = f_0 + \frac{3}{4T}$ for sequence (5).

Comparing FIG.3 and 4, it becomes obvious that intensity variations in the latter case are much weaker.

In the second and preferred embodiment for carrying out the invention the reduction in temperature effects is achieved by a combination of two or more sequences other than PAPS and NPAPS, arranged so that a definite regularity of phase alternation of RF pulses in each of the sequences is equivalent to a shift of the spectrum components of the sequences in relation to each other. At least one

of the sequences contains not less than two alternating phases and no sequences are arranged so that a definite regularity of the phase alteration of RF pulses in each of the sequences is equivalent to a shift of spectral components of the sequences in relation to each other. Further, in at least one of the sequences, there are not less than two phases that are alternating and none of the sequences contains a preparatory pulse or group of preparatory pulses.

This embodiment is intended for preferably detecting substances with a relaxation time T_1 much shorter than the duration of the pulse sequence T_{seq}.

In the case when $T_1 << T_{seq}$, the time of "phase memory" is so short that using preparatory pulses will not necessarily produce an increase of the signal intensity, and the preparatory pulse can be omitted.

For reducing temperature effects the sequences must contain pulses with various sets of the carrier frequency phases.

As before, the phase of the first pulse of each sequence is taken to be zero irrespective of its actual value. The phases of all pulses of each sequence will be determined in relation to the phase of the first pulse of this sequence.

When using a set of N ($N \geq 2$) different phases

$$\phi_1, \phi_2, \ldots \phi_i, \ldots \phi_N, \qquad (6)$$

so that all phases are within the interval from 0 to 2π radian, $\phi_i \neq \phi_j$ if $i \neq j$, and $\phi_1 = 0$, the body of each pulse sequence must contain cycles of pulses (at least one), with the pulses of each cycle containing one of the following N! sets of carrier frequency phases:

one set of phases of the following type: $\phi 1_1, \phi 1_2, \ldots \phi 1_i, \ldots \phi 1_N$;

N sets of phases of the following type: $\phi 2_1, \phi 2_2, \ldots \phi 2_i, \ldots \phi 2_{N-1}$;

: :
: :

$\frac{N!}{(N-i)!i!}$ sets of phases of the following type: ϕi_1, ϕi_2, ... ϕi_1, ... ϕi_{N-i};

: :
: :

N sets of phases of the following type: ϕN_1.

Here each phase ϕi_k $(i, k = 1, \ldots N)$ is one of the phases of set (6), with $\phi i_k \neq \phi i_m$, if $k \neq m$. Set $\phi 1_k$ is equivalent to set ϕ_k.

If sequences from one combination used in one detection process contain the same pulse phase set, they must differ by at least the sequence order of the phase alternation.

Two examples of the use of the second preferred embodiment are shown in FIG.5.

Both examples present the use of a combination of sequences without preparatory pulses for powdered RDX.

$(\varphi_x - t_{delay} - T_{acq} - \varphi_y - t_{delay} - T_{acq} - \varphi_{-x} - t_{delay} - T_{acq} - \varphi_{-y} - t_{delay} - T_{acq})_m$ and

$(\varphi_x - t_{delay} - T_{acq} - \varphi_{-y} - t_{delay} - T_{acq} - \varphi_{-x} - t_{delay} - T_{acq} - \varphi_y - t_{delay} - T_{acq})_m$.

Experiments were performed at the transition frequency $\nu_- = 3.410$ MHz at room temperature.

As in previous examples, the magnetic field component B_1 of the RF pulses equalled 4.5 Gauss. The spin-lattice relaxation time for this line was $T_1 = 11$ ms.

The difference between the two experiments shown in curves 1 and 2 in FIG.5 consists only in the difference in the receive system phase.

Keeping in mind the phases of the receiver, the sequences corresponding to curve 1 can be presented as follows:

$$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_y - t_{delay} - T_{acq(+y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)})_m; \quad (7)$$

$$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_y - t_{delay} - T_{acq(y)})_m. \quad (8)$$

Curve 2 corresponds to the combination of the same sequences but in the second sequence the phase of the receiver is changed to the opposite:

$$(\varphi_x - t_{delay} - T_{acq(+x)} - \varphi_y - t_{delay} - T_{acq(+y)} - \varphi_{-x} - t_{delay} - T_{acq(-x)} - \varphi_{-y} - t_{delay} - T_{acq(-y)})_m; \quad (9)$$

$$(\varphi_x - t_{delay} - T_{acq(-x)} - \varphi_{-y} - t_{delay} - T_{acq(+y)} - \varphi_{-x} - t_{delay} - T_{acq(+x)} - \varphi_y - t_{delay} - T_{acq(-y)})_m. \quad (10)$$

For all the four sequences: $m = 50$, $\varphi = \pi/2$; the pulse duration $t_w = 68\ \mu s$; the delay after the pulse $t_{delay} = 440 \mu s$; and the acquisition time $T_{acq(\sigma)} = 1024 \mu s$. The interval between sequences is two seconds.

The effective carrier frequencies equal:

$f_{eff} = f_0 + \frac{1}{4T}$, for sequences (7), (9); and

$f_{eff} = f_0 + \frac{3}{4T}$, for sequences (8), (10).

As a result of comparing curves 1 and 2, it is obvious that both combinations (7)-(8) and (9)-(10) show practically identical results with regards to reducing temperature effects, the only difference being an insignificant shift along the frequency axis.

It should be appreciated that the scope of the present invention is not limited to the specific embodiments described herein.

Dated this Twentieth day of June 2002.

Thorlock International Limited

Wray & Associates
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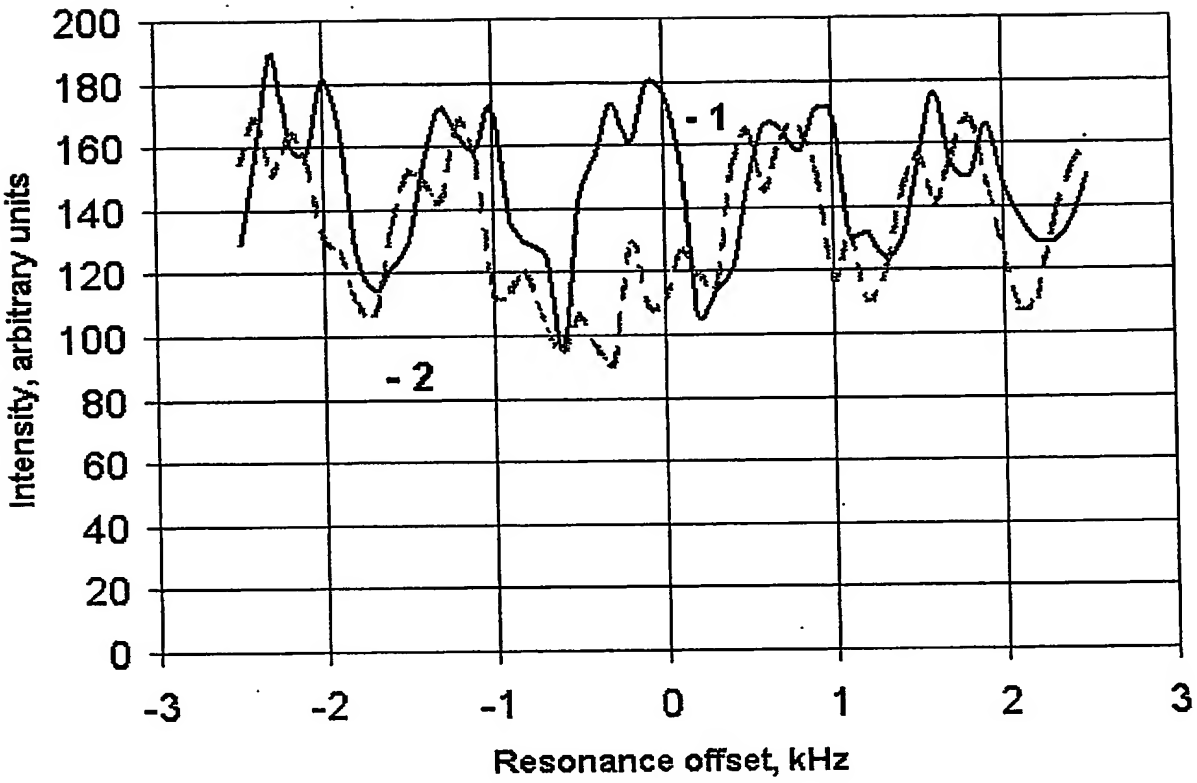
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140
120
100
80
60
40
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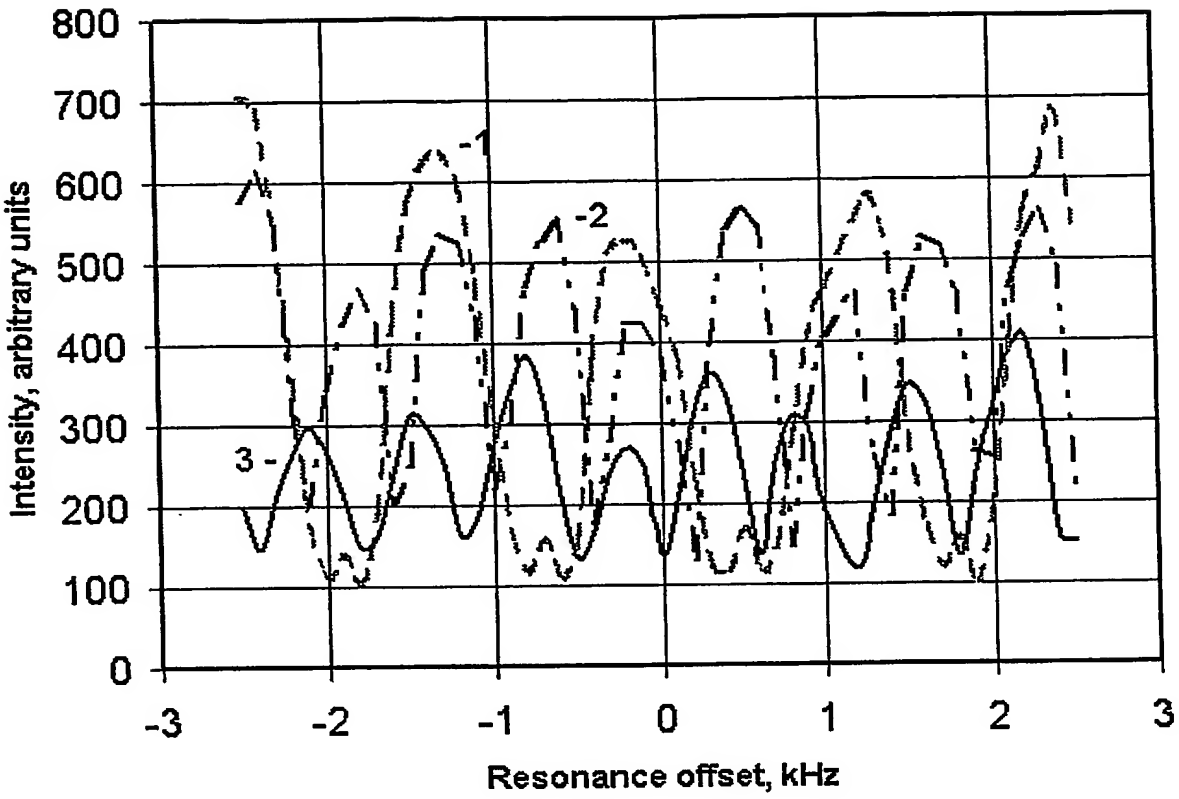
0
Intensity, arbitrary units
-3
-2
-1
0
1
2
3
Resonance offset, kHz
- 1
- 2

Fig. 1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Intensity, arbitrary units
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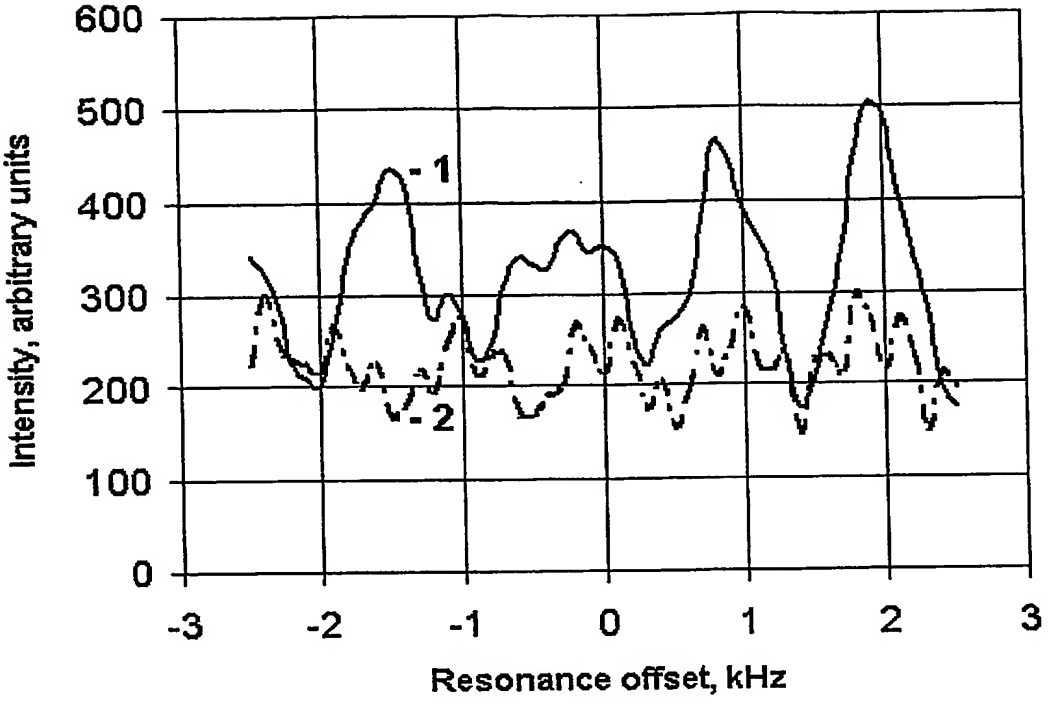
Resonance offset, kHz
-1
-2
3 -

Fig. 2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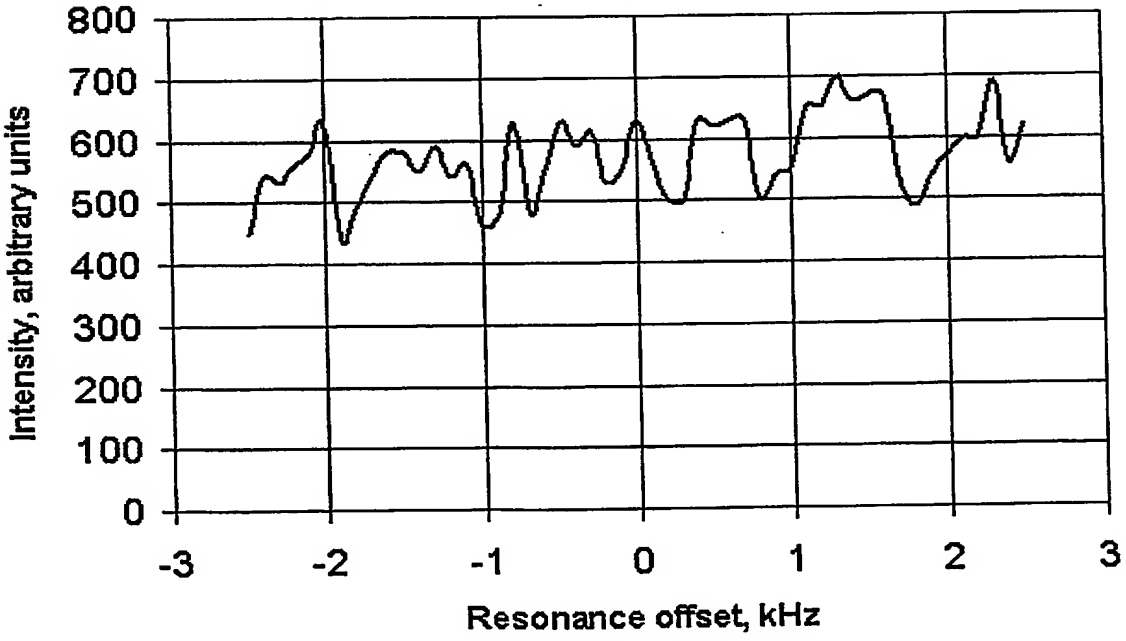
Intensity, arbitrary units
Resonance offset, kHz
- 1
- 2

Fig. 3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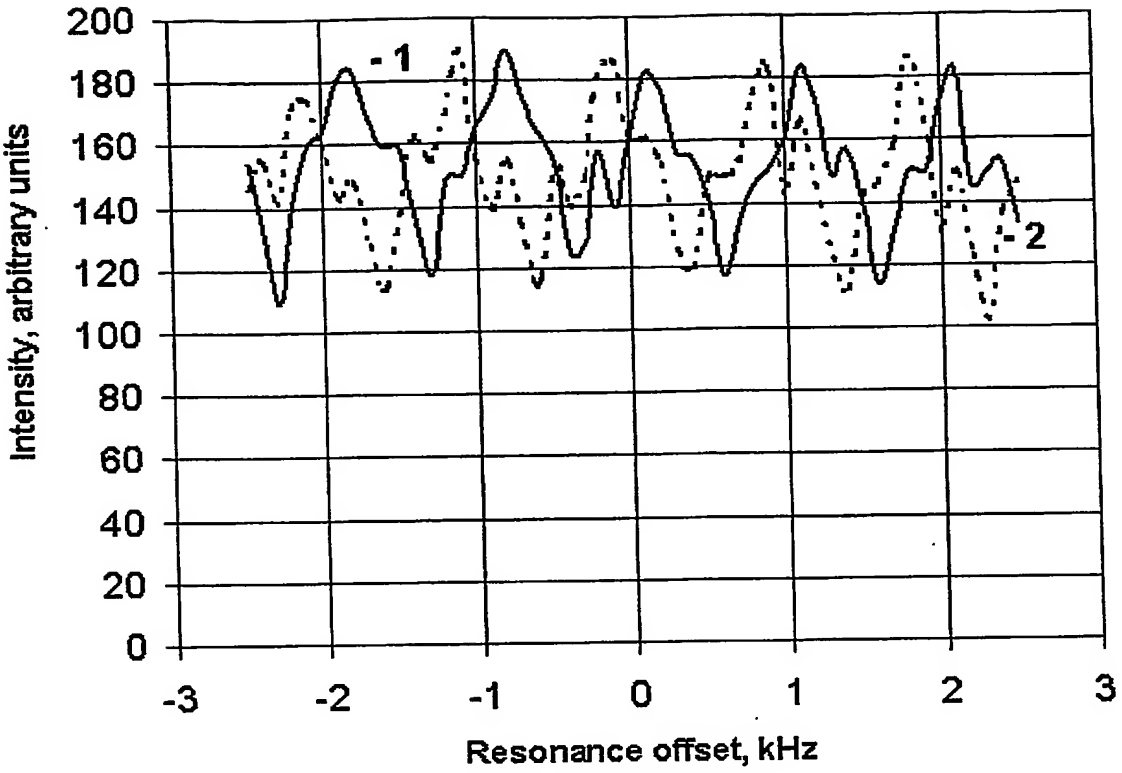
Intensity, arbitrary units
Resonance offset, kHz

Fig. 4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80
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40
20
0
Intensity, arbitrary units
-3
-2
-1
0
1
2
3
Resonance offset, kHz
-1
-2

Fig. 5